

Interfaces Involved in Modeling of Hanford Tanks

Modeling the Performance of Engineered Systems for Closure and Near-Surface Disposal Salt Lake City, Utah

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July 13 – 14, 2009









- 149 ssts with waste from fuel reprocessing
- In the process of removing waste from tanks for vitrification
- Goal to remove as much waste as possible (99 % or better)
- Permanent closure includes grouting tank void volume and placing engineered barrier over tanks and nearby infrastructure
- Components being modeled are engineered cover, waste containment system, thick vadose zone and small portion of unconfined aquifer
- First version of a contaminant flow and transport analysis has been completed and scoping process is in place with decision makers and interested parties to refine the initial effort















Engineered Cover Features

- Primary Purpose: Infiltration Control
- Supporting Performance Information
 - 20 + Years of Studying Infiltration/Barriers
 - Field Lysimeters
 - Prototype Barrier at B-57 Crib
 - Chlorine Studies
 - May Change Final Design to Mono-Layer
- Modeling Approach
 - Averaged Annual Infiltration Rate
 - Uses Design Goal of 0.5 mm/y
 - Measured a B-57 Prototype is < 0.1 mm/yr



Barrier: Potential Grouted Tank Structure

Waste Containment System

- Features (Waste inside liner, concrete shell, and grouted void volume)
- Primary Purpose: Limit water interaction with waste to slow release
- Supporting Performance Information
 - Generic diffusion release (SRL, Harbour et al. 2004 provided effective diffusion coefficients for Tc-99)
 - Durability of grout (SRL, Harbour et al. 2005 provided insights through consideration of ancient structures [Pantheon, Hadrian's Wall, and Roman Aqueducts)
 - Initiated Waste Release Studies at PNNL
 - Release of contaminants from residual waste
 - Interaction between residual waste and stabilizing grout
- Modeling Approach
 - Diffusional release at the structure bottom vadose zone interface
 - Assumes steel liner goes away at closure (conservative approach → no data for how the steel liner behaves)





Vadose Zone

- Features
 - Greater than 200 ft thick
 - Three major stratigraphic units
 - Ubiquitous finer stratification of alternating particle size distribution, low moisture content (0.03 to 0.12 volumetric moisture content)
- Supporting Performance Information
 - Unsaturated/saturated hydraulic conductivity measurements on lab scale samples for major particle size distributions
 - Hanford site specific moisture characteristic curves (van Genuchten-Mualem Parameters)
 - Geophysical logging has provided volumetric moisture content
 - Hanford site specific sorption data for various contaminants (mostly radionuclide)
- Modeling Approach
 - Moisture-dependent hydraulic conductivity and anisotropy,
 - Two-dimensional simulation
 - Advective flow through porous media





Unconfined Aquifer

- Features
 - Location dependent major unit
 - Hydraulic conductivity
 - Thickness
 - Gradient
- Supporting Performance Information
 - In -situ hydraulic conductivity measurements
 - Head data from monitoring well network
- Modeling Approach
 - Advective flow through porous media









Post -closure conditions affecting flow and transport of tank residual contaminants

- Small residual inventory for mobile contaminants (e.g. ranges from ~0 to 12 Ci of Tc-99, at WMA C maximum = ~0.75 Ci
- Recharge History
 - Operational Period: 2000-2032: 100 mm/yr
 - Functional Surface Barrier: 2032-2532: 0.5 mm/yr
 - Degraded Surface Barrier: 2532-12,032: 1.0 mm/yr
- Diffusion release from tank bottom (1E-9 cm^2/s)
- Vadose zone > 200 ft thick
- Contaminant sorption bins in vadose zone and unconfined aquifer (0, 0.2, 0.6 mL/g)
- High groundwater flux in local unconfined aquifer (200 East Area)

Schematic Diagram of Subsurface Contaminant Migration Under an SST WMA



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Typical Result at WMA Boundary Groundwater Pathway



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- Within 10,000 yr post-closure, non negligible radionuclide groundwater concentrations from tank residuals come only from completely mobile (Kd = 0 mL/g) contaminants
- Contamination levels are proportional to inventory and only Tc-99 has sufficient estimated inventory (< 3 Ci per pathline row) to generate non negligible groundwater concentrations
- Peak concentrations are more than 2 orders of magnitude below the MCL of 900 pCi/L at the fenceline